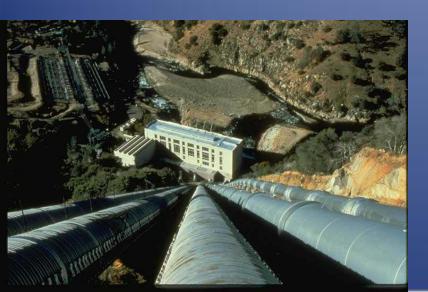
ASCE Manual and Reports on Engineering Practice No. 79

Steel Penstocks

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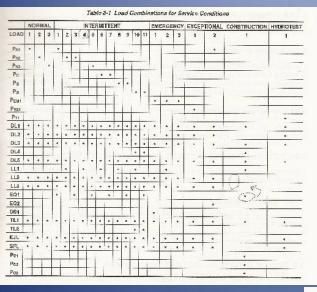


MOP 79 Steel Penstocks Current Status

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- 3. Design Criteria and Allowable Stresses
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- 6. Steel Tunnel Liners
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Design Considerations







Exposed Control and Familia Employ						
CATEGORY	TYPE	100% RT or UT	SPOT RT1	NO RT OR UT ²		
LONGITUDINAL BUTT WELDS CIRCUMFERENTIAL BUTT WELDS SPIRAL (HELICAL) BUTT WELDS	DOUBLE-WELDED BUTT JOINTS	1.00	.85	.70		
	SINGLE-WELDED BUTT JOINTS WITH BACKING STRIPS	.90	.80	.65		
	SINGLE-WELDED BUTT JOINT WITHOUT BACKING STRIPS (CIRCUMFERENTIAL ONLY, <5/8 in. THICK AND <24 in. O.D. ⁴)	NA ³	NA.	.60		
DOUBLE FULL-FILLET LAP	LONGITUDINAL toux = 3/8 in.	NA NA	NA	.55		
	CIRCUMFERENTIAL trax = 5/8 in.	NA NA	NA.	.66		
SINGLE FULL-FILLET LAP JOINTS WITH PLUG WELDS	CIRCUMFERENTIAL ONLY, FOR <24 in. O.D. Inner = 1/2 in.	NA	NA	.50		

Buried Penstocks

CATEGORY	TYPE	100% RT OR UT	SPOT RT1	NO RT OR UT2
LONGITUDINAL BUTT WELDS CIRCUMFERENTIAL BUTT WELDS SPIRAL (HELICAL) BUTT WELDS	DOUBLE-WELDED BUTT JOINTS	1.00	.85	.70
	SINGLE-WELDED BUTT JOINTS WITH BACKING STRIPS	.90	.80	.65
	SINGLE-WELDED BUTT JOINTS WITHOUT BACKING STRIPS (CIRCUMFERENTIAL ONLY, <5/8 in. THICK AND <24 in. O.D.)	NA.	NA	.60
DOUBLE FULL-FILLET LAP	LONGITUDINAL tmax = 3/8 in.	NA.	NA.	.55
	CIRCUMFERENTIAL 1 _{max} = 5/8 in.	NA NA	NA.	.55
SINGLE FULL-FILLET LAP JOINTS WITH PLUG WELDS	CIRCUMFERENTIAL ONLY, FOR < 24 in. O.D. I _{mel} = 5/8 in.	NA NA	NA	.50
BELL-AND-SPIGOT JOINTS	SINGLE FILLET LIMITED TO Innex = 5/8 in.	NA NA	NA	.45
	DOUBLE FILLET t _{max} = 5/8 in.	NA	NA	.55

Table 3-2 SI Classifications for Typical Parts Found in Penstocks and Tunnel Liners

CASE	SI CATEGO	
RING GIRDER SUPPORTS AND STIFFENER RINGS		
RIM BENDING	Q	
LOCAL MEMBRANE HOOP STRESS IN THE PENSTOCK IN THE CIRCUMFERENTIAL DIRECTION		
BENDING STRESSES IN RING GIRDER AND/OR STIFFENERS ACTING ACROSS THE DEPTH OF THE GIRDER	Pn	
BENDING + AXIAL SI IN RING	P _n	
RIM BENDING IN THE PENSTOCK SHELL PLUS DIRECT/AXIAL LOAD	(Q+P _n)	
SADDLES (PENSTOCK SHELL IMMEDIATELY ABOVE HORN OF SADDLE)	in a second	
HORIN BENDING	Q	
HORN HOOP MEMBRANE LOAD	Pi,	
SHEAR IN SHELL ADJACENT TO HORN	0.65	
BEARING OR COMPRESSION FROM BEARING LOADS	Per	
BENDING IN BASE PLAYES AND SADDLE PLATES ACROSS THICKNESS OF ELEMENT	Pb	
LOADED ATTACHMENTS AND NOZZLES		
MEMBRANE SI IN SHELL OF PENSTOCK DUE TO THE LOADS	PL	
BENDING SI IN SHELL OF PENSTOCK DUE TO THE LOADS	Q	
NOZZLE NECKS		
NOZZLE NECKS OUTSIDE LIMITS OF REINFORCEMENT FROM EXTERNAL LOADS AND MOMENTS, AND PRESSURE	PL	
NOZZLE NECKS WITHIN LIMITS OF REINFORCEMENT FROM EXTERNAL LOADS AND MOMENTS, AND PRESSURE	Pm	
BIFURCATIONS		
MEMBRANE STRESS INTENSITY AWAY FROM REINFORCING GIRDERS AND AWAY FROM CHANGES IN DIRECTION	Pn	
MEMBRANE STRESS INTENSITY ADJACENT TO REINFORCING GIRDERS AND CHANGES IN DIRECTION		
BENDING STRESS ACROSS THICKNESS OF SHELL		
MAXIMUM STRESS INTENSITY IN REINFORCING GIRDERS	Pa + PL	
MISCELLANEOUS		
MEMBRANE HOOP STRESS FROM INTERNAL PRESSURE IN CYLINDRICAL AND CONICAL PENSTOCK SECTIONS AND FOR FORMED SHELLS AWAY FROM DISCONTINUITIES		
MEMBRANE SI IN THE VICINITY OF ATTACHMENTS UNDER LOAD, HORN AREA OF SADDLE SUPPORTS, CONICAL- TO-CYLINDRICAL INTERSECTIONS, AND PENSTOCK SHELLS ADJACENT TO NOZZLES		
BENDING SI IN FLAT HEADS AND COVERS	Pb	
TEMPERATURE SI	0	





Intended Use of MOP 79

A Penstock is defined in MOP 79 as a pressurized, closed water conduit located between the first free water surface and a hydroelectric power/pump station.



Risk Assessment

Chapter 16 - Maintenance

An estimate of the potential risks associated with penstock failure mechanisms must be developed. This type of assessment is site dependant and must include, but not be limited to, estimating potential failure modes, assessing the probability or likelihood of such an event, and assessing the potential for loss of life and damage associated with each identified failure mode.



Engineering VS Operation

- Safety
- Operating efficiency
- Cost
- Installation restraints
- Repair and maintenance
- Environmental concerns



